



COLLÈGE
DE FRANCE
—1530—



Chaire de Physique Mésoscopique
Michel Devoret
Année 2008, 13 mai - 24 juin

CIRCUITS ET SIGNAUX QUANTIQUES

QUANTUM SIGNALS AND CIRCUITS

Cinquième Leçon / *Fifth Lecture*

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08-V-1

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<http://www.college-de-france.fr>

and follow links to:

<http://www.physinfo.fr/lectures.html>

[PDF FILES OF ALL LECTURES WILL BE POSTED ON THIS WEBSITE](#)

Questions, comments and corrections are welcome!

08-V-2

CALENDAR OF SEMINARS

May 13: Denis Vion, (Quantronics group, SPEC-CEA Saclay)

Continuous dispersive quantum measurement of an electrical circuit

May 20: Bertrand Reulet (LPS Orsay)

Current fluctuations : beyond noise

June 3: Gilles Montambaux (LPS Orsay)

Quantum interferences in disordered systems

June 10: Patrice Roche (SPEC-CEA Saclay)

Determination of the coherence length in the Integer Quantum Hall regime

June 17: Olivier Buisson, (CRTBT-Grenoble)

A quantum circuit with several energy levels

June 24: Jérôme Lesueur (ESPCI)

High Tc Josephson Nanojunctions: Physics and Applications

08-V-3

PROGRAM OF THIS YEAR'S LECTURES

Lecture I: Introduction and overview

Lecture II: Modes of a circuit and propagation of signals

Lecture III: The "atoms" of signal

Lecture IV: Quantum fluctuations in transmission lines

Lecture V: Introduction to non-linear active circuits

Lecture VI: Amplifying quantum signals with dispersive circuits

08-V-4

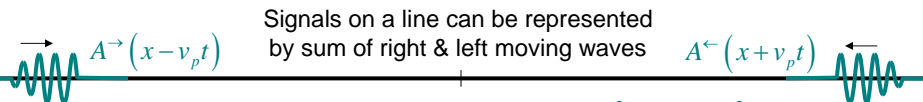
LECTURE V : INTRODUCTION TO NON-LINEAR ACTIVE CIRCUITS

OUTLINE

1. Where we stand so far, purpose of this lecture
2. Fluctuations of damped harmonic oscillator
3. Hamiltonian approach of Caldeira and Leggett
4. Properties of scattering matrix
5. Non-linear active circuits

08-V-5

1ST QUANTIZATION OF SIGNALS (CLASSICAL WAVES)



Energy flux @ $x = 0$: $\mathcal{P}(t) = |A^>(t)|^2 - |A^<(t)|^2$

Decomposition
of signal into modes:

$$A_{mp}^{\rightleftharpoons} = \int_{-\infty}^{+\infty} dt \psi_{mp}^*(t) A^{\rightleftharpoons}(t)$$

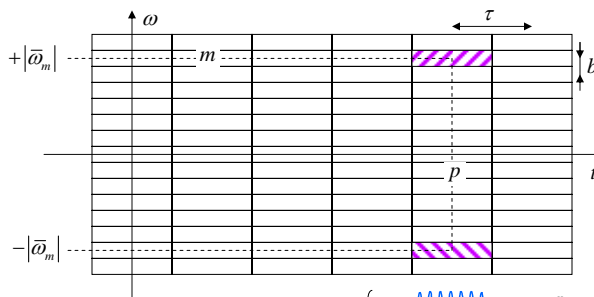
$$A_{-mp}^{\rightleftharpoons} = (A_{mp}^{\rightleftharpoons})^*$$

$$[A_{mp}^{\rightleftharpoons}] = [\text{energy}]^{1/2}$$

Each mode is a
"flying oscillator":

$$\left\{ A_{m_1 p_1}^{\rightleftharpoons}, A_{m_2 p_2}^{\rightleftharpoons} \right\}_{\text{P.B.}} = -\frac{i}{2} \bar{\omega}_{m_1} \delta_{m_1+m_2} \delta_{p_1-p_2}$$

INFORMATION OF OSCILLATORS
IS CONSERVED



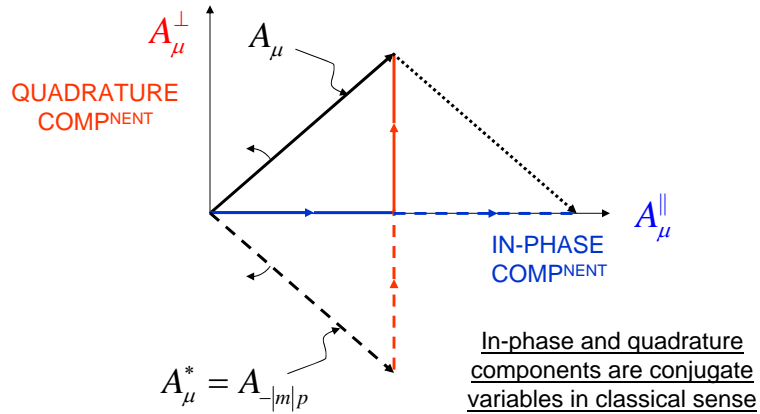
$$\psi_{mp}(t) \begin{cases} \text{---} \text{cos} \text{---} & \text{"cos"} \\ +i \times & \\ \text{---} \text{sin} \text{---} & \text{"sin"} \end{cases}$$

$$\int_{-\infty}^{+\infty} dt \psi_{m_1 p_1}^*(t) \psi_{m_2 p_2}(t) = \delta_{m_1 m_2} \delta_{p_1 p_2}$$

08-V-6c

1ST QUANTIZATION OF SIGNALS: FRESNEL REPRESENTATION OF MODE

mode index $\mu = \{|m|, p, \rightarrow \text{ or } \leftarrow\}$ refers to a pair of tiles



08-V-7

2ND QUANTIZATION OF SIGNALS (QUANTUM WAVES)

classical mode amplitude $A_{mp}^{\rightleftharpoons} \rightarrow \hat{A}_{mp}^{\rightleftharpoons}$ quantum operator

Poisson bracket $\{A_{m_1 p_1}^{\rightleftharpoons}, A_{m_2 p_2}^{\rightleftharpoons}\}_{P.B.} \rightarrow [\hat{A}_{m_1 p_1}^{\rightleftharpoons}, \hat{A}_{m_2 p_2}^{\rightleftharpoons}] = \frac{\hbar \bar{\omega}_{m_1}}{2} \delta_{m_1+m_2} \delta_{p_1-p_2}$ commutator

physical observables

continuous field variables

continuous field ladder operators:
(N.B.: arrows have been dropped)

$$\hat{a}[\omega = \omega_m] = \lim_{b \rightarrow 0} \frac{1}{\sqrt{b \frac{\hbar |\omega|_m}{2}}} \hat{A}_{mp}$$

commutator of \hat{a} 's: $[\hat{a}[\omega_1], \hat{a}[\omega_2]] = \text{sg}(\omega_1 - \omega_2) \delta[\omega_1 + \omega_2]$

average value of anticommutator in thermal state: $\langle \{\hat{a}[\omega_1], \hat{a}[\omega_2]\} \rangle_T = \coth \frac{\hbar |\omega_1|}{2k_B T} \delta[\omega_1 + \omega_2]$

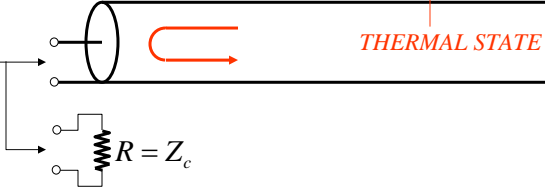
08-V-8a

QUANTUM FLUCTUATION-DISSIPATION THEOREM

$$\langle \hat{V}^\omega[\omega_1] \hat{V}^\omega[\omega_2] \rangle = S_{VV}^\omega[\omega] \delta(\omega_1 + \omega_2)$$

$$S_{VV}^\omega[\omega] = \frac{Z_c}{4} \hbar \omega \left[\coth\left(\frac{\hbar \omega}{2k_B T}\right) + 1 \right]$$

$$S_{VV}[\omega] = R \hbar \omega \left[\coth\left(\frac{\hbar \omega}{2k_B T}\right) + 1 \right]$$



$$S_{VV}[\omega] = 4S_{VV}^\omega[\omega]$$

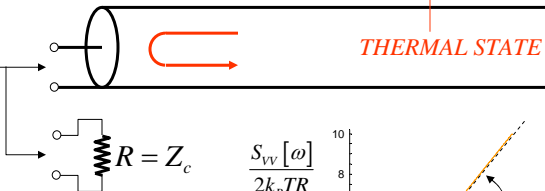
08-V-8a

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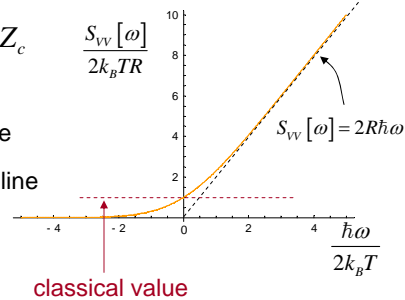
$$S_{VV}[\omega] = R \hbar \omega \left[\coth\left(\frac{\hbar \omega}{2k_B T}\right) + 1 \right]$$



$$S_{VV}[\omega] = 4S_{VV}^\omega[\omega]$$

QUANTUM
ASYMMETRY
OF
FLUCTUATIONS

$\omega > 0$: emission into the line
 $\omega < 0$: absorption from the line



08-V-8b

QUANTUM FLUCTUATION-DISSIPATION THEOREM

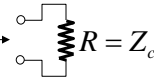
$$\langle \hat{V}^\omega[\omega_1] \hat{V}^\omega[\omega_2] \rangle = S_{VV}^\omega[\omega] \delta(\omega_1 + \omega_2)$$

$$S_{VV}^\omega[\omega] = \frac{Z_c}{4} \hbar \omega \left[\coth\left(\frac{\hbar \omega}{2k_B T}\right) + 1 \right]$$

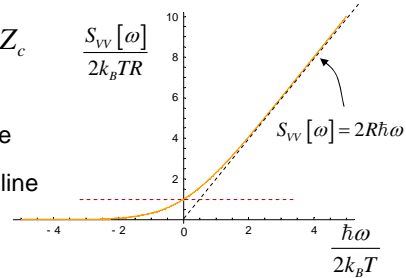
$$S_{VV}[\omega] = R \hbar \omega \left[\coth\left(\frac{\hbar \omega}{2k_B T}\right) + 1 \right]$$



$$S_{VV}[\omega] = 4S_{VV}^\omega[\omega]$$



$$\frac{S_{VV}[\omega]}{2k_B T R}$$



QUANTUM
ASYMMETRY
OF
FLUCTUATIONS

$\omega > 0$: emission into the line

$\omega < 0$: absorption from the line

Recover results of Johnson-Nyquist noise:

Voltage fluctuations in classical regime:

$$\mathcal{S}_{VV}[\nu] = 4k_B T R$$

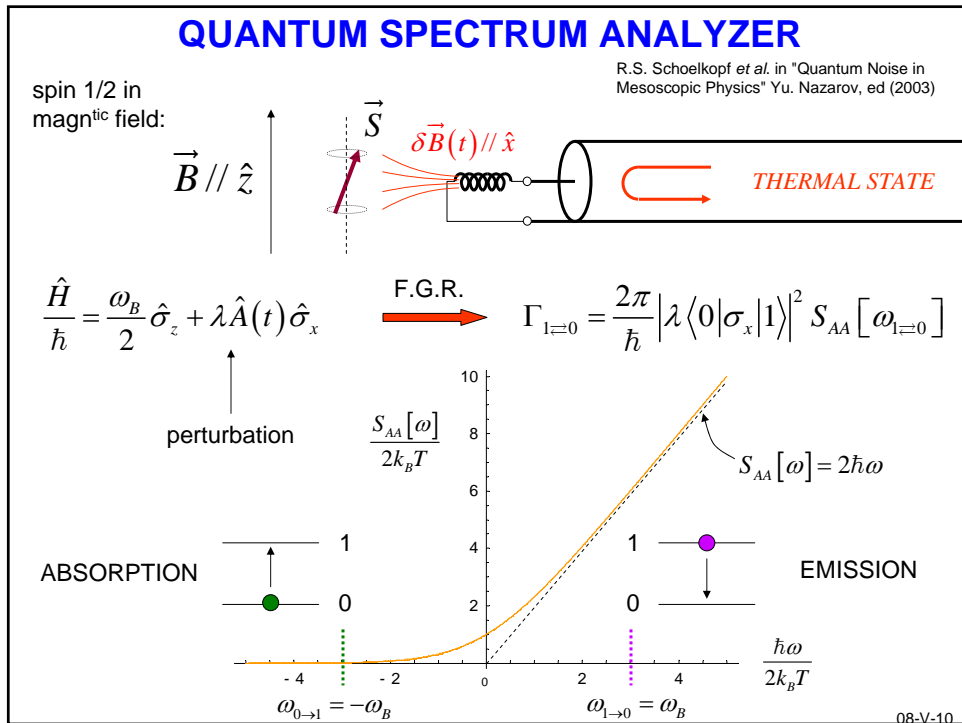
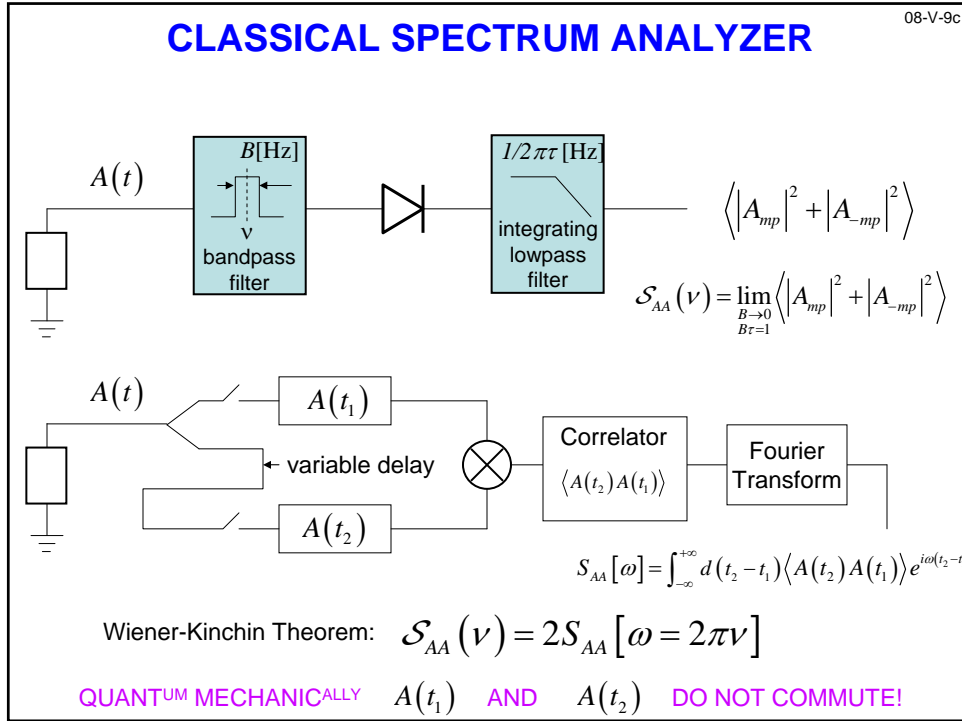
Line power flow in classical regime:

$$P = k_B T B \quad (k_B T \text{ per mode})$$

08-V-8c

CAN WE BUILD A
QUANTUM SPECTRUM ANALYZER?

08-V-8d



PURPOSE OF THIS LECTURE

WHAT IS THE EFFECT OF THE QUANTUM PART OF
FLUCTUATIONS?

DIFFERENT CLASSES
OF RESPONSE OF CIRCUITS

DISPERSIVE vs DISSIPATIVE

PASSIVE vs ACTIVE

LINEAR vs NON-LINEAR

08-V-11

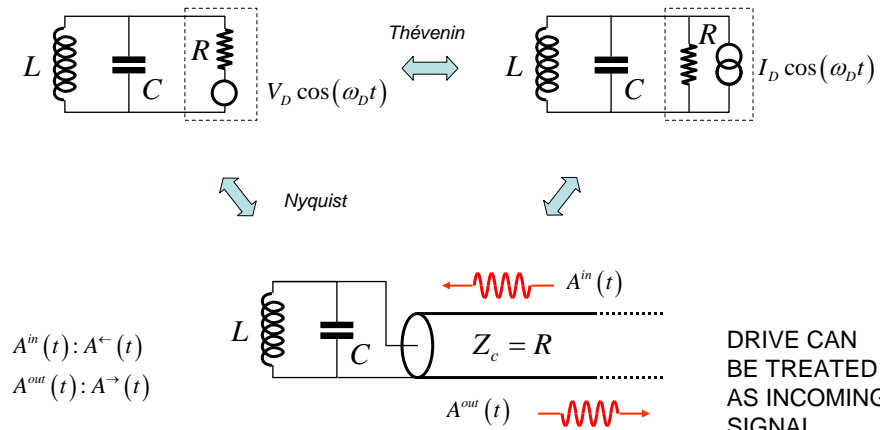
OUTLINE

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08-V-5b

SCATTERING APPROACH TO DRIVEN DISSIPATIVE CIRCUITS

MAIN IDEA: RESISTANCE IS EQUIVALENT TO SEMI-INFINITE TRANSMISSION LINE



08-V-12a

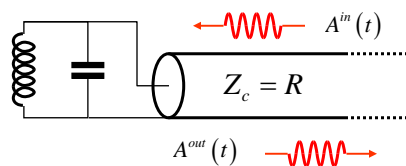
A KEY IDEA

$$\leftarrow \text{wavy arrow} \quad A^-(t)$$

$$Z_c = R$$

$$A^+(t) \rightarrow \text{wavy arrow}$$

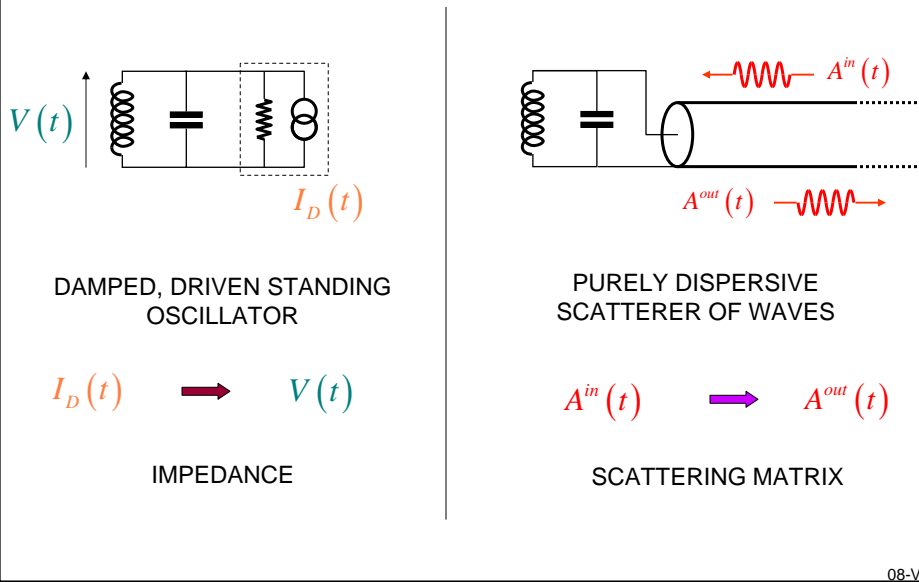
UNLIKE $A^-(t)$ AND $A^+(t)$, $A^in(t)$ AND $A^out(t)$ ARE NOT INDEPENDENT



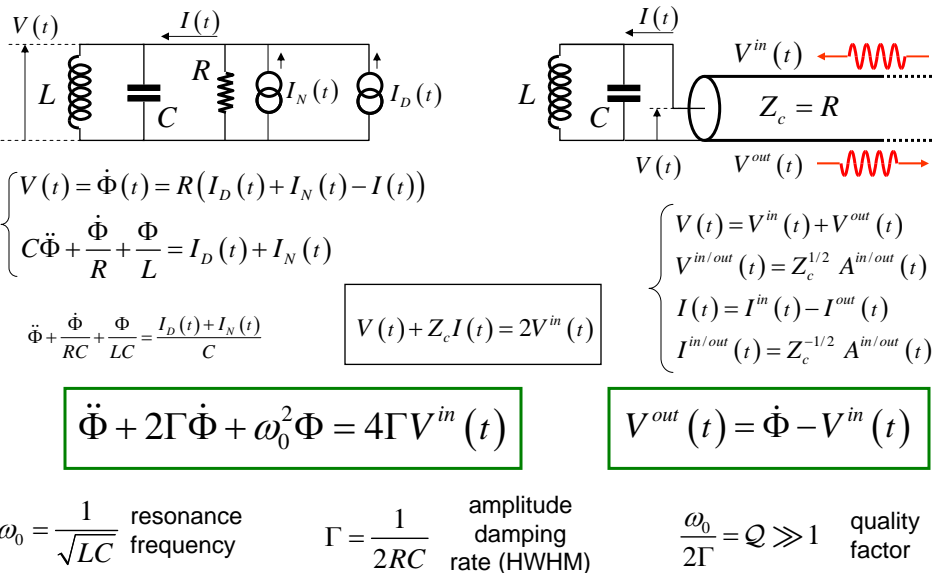
TERMINATING CIRCUIT IMPOSES A STRICT RELATIONSHIP BETWEEN INCOMING AND OUTGOING WAVES

08-V-13

SAME CIRCUIT, DIFFERENT POINTS OF VIEW



RESISTANCE-TRANSMISSION LINE EQUIVALENCE



INPUT-OUTPUT RELATION IN OPERATOR FORM

$$\ddot{\Phi} + 2\Gamma\dot{\Phi} + \omega_0^2\Phi = 4\Gamma V^{in}(t)$$

$$V^{out}(t) = \dot{\Phi} - V^{in}(t)$$

$$\frac{d^2}{dt^2}\hat{\Phi} + 2\Gamma\frac{d}{dt}\hat{\Phi} + \omega_0^2\hat{\Phi} = 4\Gamma\hat{V}^{in}(t)$$

$$\hat{V}^{out}(t) = \frac{d}{dt}\hat{\Phi} - \hat{V}^{in}(t)$$

Fourier domain:

$$(\omega_0^2 - \omega^2 + 2i\omega\Gamma)\hat{\Phi}[\omega] = 4\Gamma\hat{V}^{in}[\omega]$$

$$\hat{V}^{out}[\omega] = i\omega\hat{\Phi}[\omega] - \hat{V}^{in}[\omega]$$

$$\hat{V}^{out}[\omega] = -\frac{\omega_0^2 - \omega^2 - 2i\omega\Gamma}{\omega_0^2 - \omega^2 + 2i\omega\Gamma}\hat{V}^{in}[\omega]$$

UNIT MODULUS COMPLEX NUMBER

08-V-16a

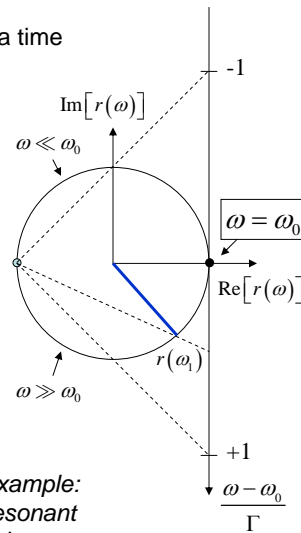
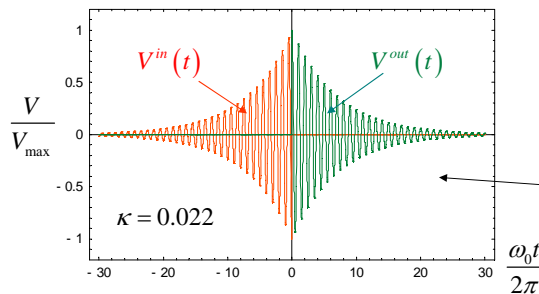
ROTATING WAVE APPROXIMATION

Since $\frac{\Gamma}{\omega_0} = \kappa = \frac{1}{2Q} \ll 1$ we can consider 1 pole at a time

$$r(\omega) = -\frac{\omega_0^2 - \omega^2 - 2i\omega\Gamma}{\omega_0^2 - \omega^2 + 2i\omega\Gamma} \simeq \frac{1 - i\frac{\omega - \omega_0}{\Gamma}}{1 + i\frac{\omega - \omega_0}{\Gamma}}$$

$\omega > 0; r(-|\omega|) = r(|\omega|)^*$

$$V[\omega] = (1 + r[\omega])V^{in}[\omega] \simeq \frac{2}{1 + i\frac{\omega - \text{sgn}(\omega)\omega_0}{\Gamma}}V^{in}[\omega]$$



example:
resonant
drive

08-V-17c

FLUCTUATIONS OF THE RESISTIVELY DAMPED LC RESONATOR

$$\begin{aligned} \langle \hat{\Phi}[-\omega] \hat{\Phi}[\omega] \rangle &= \frac{|1+r(|\omega|)|^2}{\omega^2} S_{VV}^{in}[\omega] \\ &= Z_c \frac{|1+r(|\omega|)|^2}{\omega^2} \left(\frac{\hbar\omega}{2} \coth \frac{\hbar\omega}{2k_B T} \right) \end{aligned}$$

$$\langle \hat{\Phi}^2 \rangle = \frac{1}{2\pi} \int_{-\infty}^{+\infty} d\omega \langle \hat{\Phi}[-\omega] \hat{\Phi}[\omega] \rangle \quad \text{converges}$$

$$\langle \hat{Q}^2 \rangle = \frac{1}{2\pi Z_0^2} \int_{-\infty}^{+\infty} d\omega \omega^2 \langle \hat{\Phi}[-\omega] \hat{\Phi}[\omega] \rangle \quad \text{diverges !}$$

$$Z_0 = \sqrt{\frac{L}{C}}$$

08-V-18a

FLUX FLUCTUATIONS OF THE DAMPED LC RESONATOR

INTEGRAL CAN BE PERFORMED ANALYTICALLY AND YIELD MEANINGFUL RESULTS

H. Grabert, U. Weiss and P. Talkner, Z. Phys. B 55 (1984) 87

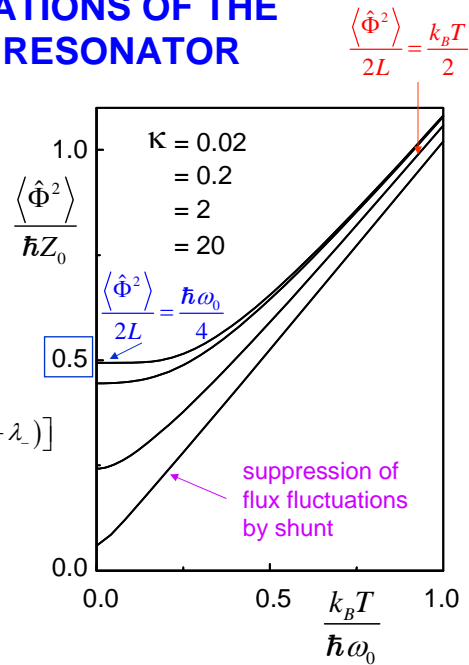
dimensionless fluctuations

dimensionless temperature

$$\frac{\langle \hat{\Phi}^2 \rangle}{\hbar Z_0} = \frac{k_B T}{\hbar \omega_0} + \frac{1}{2\pi\sqrt{\kappa^2 - 1}} [\Psi(1+\lambda_+) - \Psi(1+\lambda_-)]$$

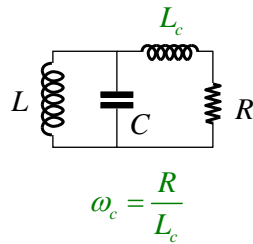
$\Psi(x)$ is polygamma function

$$\lambda_{\pm} = \frac{\kappa \pm \sqrt{\kappa^2 - 1}}{2\pi k_B T / (\hbar \omega_0)}$$



08-V-19a

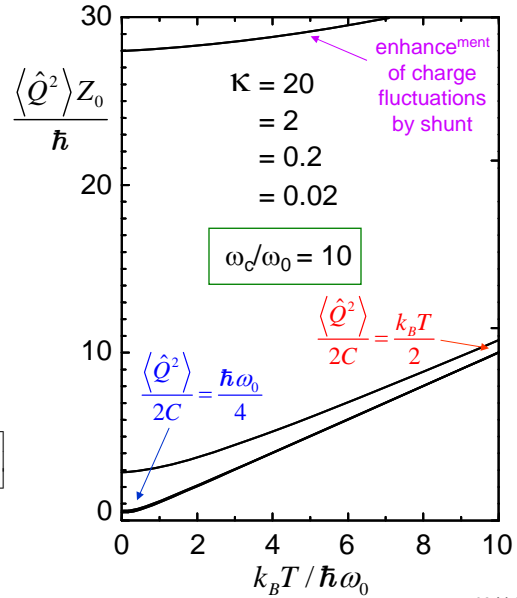
CHARGE FLUCTUATIONS OF THE DAMPED LC RESONATOR WITH INDUCTIVE CUTOFF



$$\langle \hat{Q}^2 \rangle = \frac{1}{Z_0^2} \langle \hat{\Phi}^2 \rangle + \Delta_c$$

$$\Delta_c = \frac{\hbar \kappa}{\pi Z_0} \left[2\Psi(1+\lambda_c) - \frac{1}{\sqrt{\kappa^2 - 1}} [\lambda_+ \Psi(1+\lambda_+) - \lambda_- \Psi(1+\lambda_-)] \right]$$

$$\lambda_{\pm} = \frac{\hbar \omega_0}{2\pi k_B T} \left(\frac{\omega}{\omega_c} - 2\kappa \right)$$



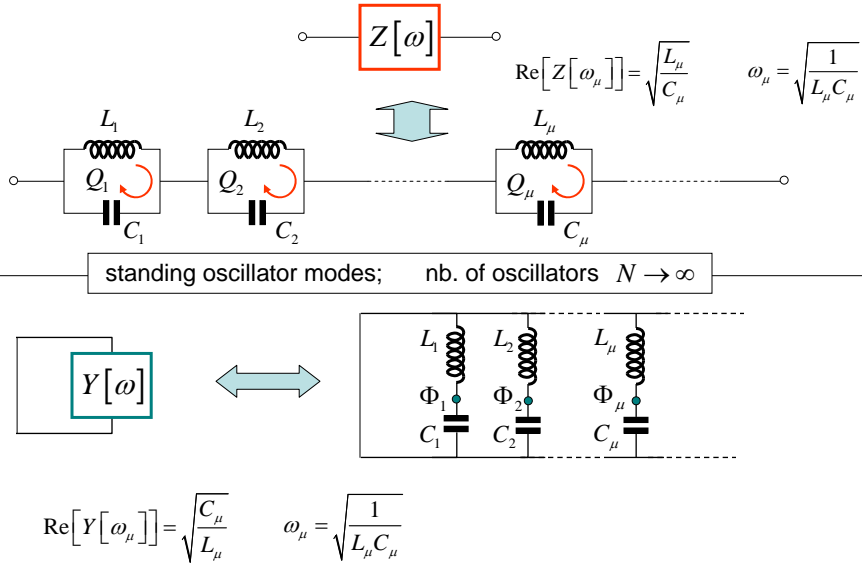
08-V-20a

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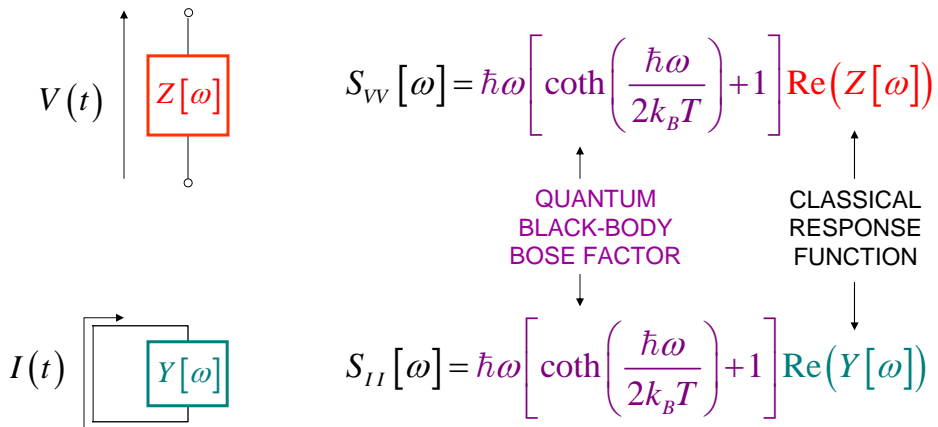
08-V-5c

ANOTHER POINT OF VIEW: HAMILTONIAN APPROACH OF CALDEIRA AND LEGGETT



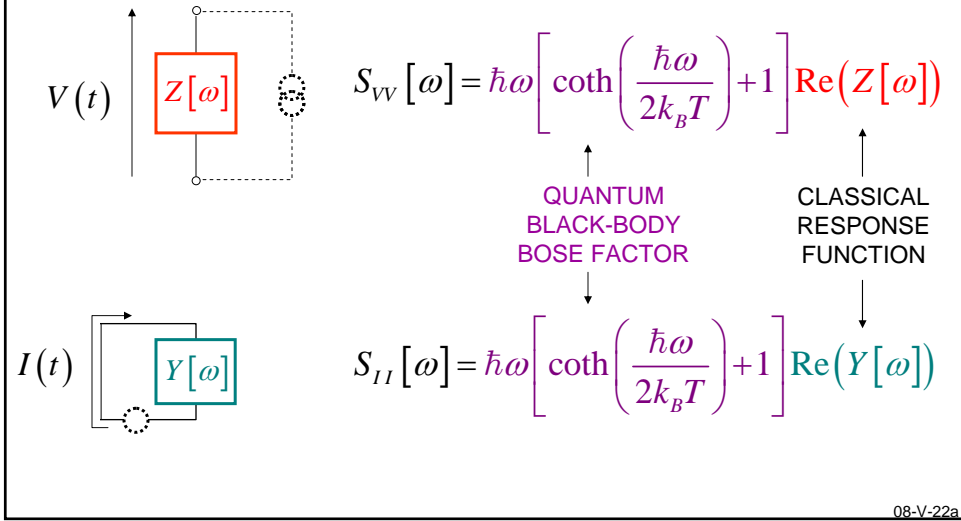
08-V-21a

GENERALIZATION OF QUANTUM FLUCTUATION-DISSIPATION THEOREM TO ARBITRARY IMPEDANCE OR ADMITTANCE

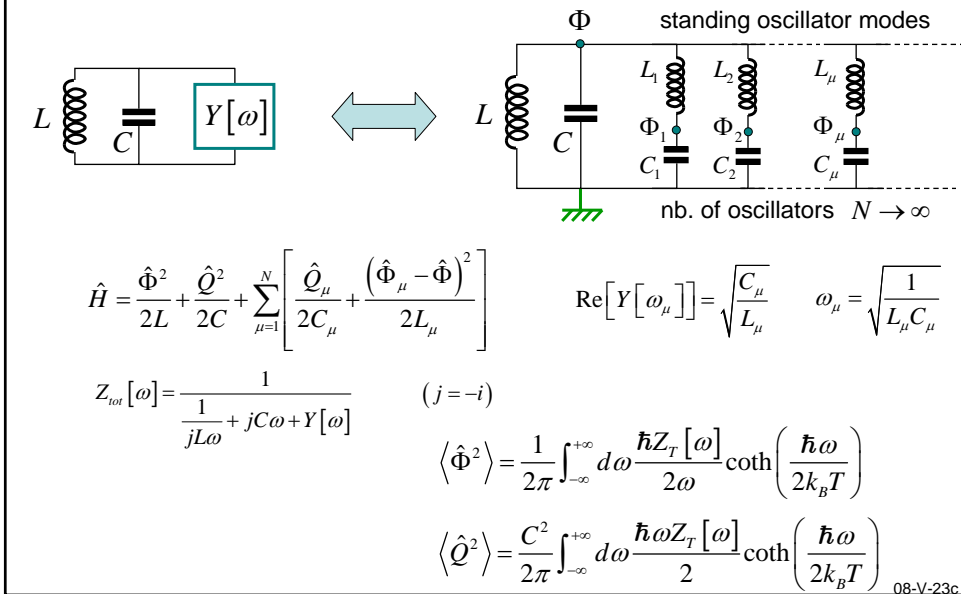


08-V-22

GENERALIZATION OF QUANTUM FLUCTUATION- DISSIPATION THEOREM TO ARBITRARY IMPEDANCE OR ADMITTANCE



FLUCTUATIONS OF OSCILLATOR FOR AN ARBITRARY ADMITTANCE



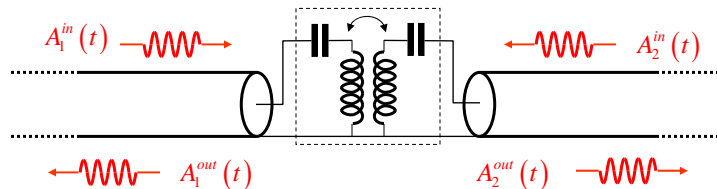
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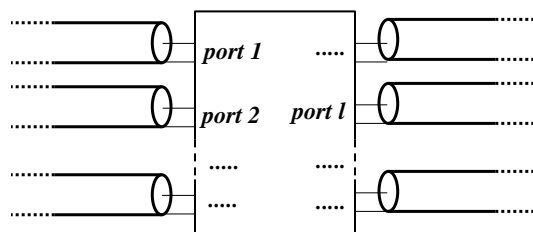
08-V-5d

MULTIPLE PORT CIRCUITS

Example:



In general:



08-V-24a

SCATTERING MATRIX FOR PASSIVE LINEAR CIRCUIT

$$\begin{matrix}
 \begin{bmatrix} A_1^{out}[\omega] \\ A_2^{out}[\omega] \\ \dots \\ A_l^{out}[\omega] \\ \dots \end{bmatrix} \\
 \uparrow \\
 \text{OUTGOING} \\
 \text{AMPLITUDES}
 \end{matrix}
 =
 \begin{matrix}
 \begin{bmatrix} s_{11}[\omega] & s_{12}[\omega] & \dots & s_{1l}[\omega] & \dots \\ s_{21}[\omega] & s_{22}[\omega] & \dots & s_{2l}[\omega] & \dots \\ \dots & \dots & \dots & \dots & \dots \\ s_{l1}[\omega] & s_{l2}[\omega] & \dots & s_{ll}[\omega] & \dots \\ \dots & \dots & \dots & \dots & \dots \end{bmatrix} \\
 \uparrow \\
 \text{"S" PARAMETERS,} \\
 \text{SCATTERING MATRIX}
 \end{matrix}
 \begin{matrix}
 \begin{bmatrix} A_1^{in}[\omega] \\ A_2^{in}[\omega] \\ \dots \\ A_l^{in}[\omega] \\ \dots \end{bmatrix} \\
 \uparrow \\
 \text{INCOMING} \\
 \text{AMPLITUDES}
 \end{matrix}
 \end{matrix}$$

same frequency

CAUSALITY \Rightarrow POLES OF S MATRIX IN LOWER-HALF PLANE

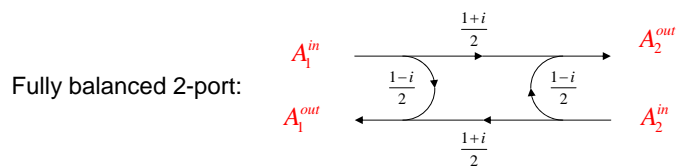
INFORMATION CONSERVATION + ENERGY CONSERVATION \Rightarrow UNITARITY OF S MATRIX $\boxed{S^\dagger S = 1}$

08-V-25a

SCATTERING MATRIX FOR NON-DISSIPATIVE LINEAR 2-PORT

$$S = \begin{bmatrix} e^{i\alpha}|r| & e^{i\beta}\sqrt{1-r^2} \\ e^{i\gamma}\sqrt{1-r^2} & e^{i\delta}|r| \end{bmatrix}$$

Unitarity constraint: $\alpha + \delta - \beta - \gamma = \pi \text{ mod } 2\pi$



~~$$\begin{bmatrix} \cos \vartheta & i \sin \vartheta \\ -i \sin \vartheta & \cos \vartheta \end{bmatrix}$$~~

$$\begin{bmatrix} \cos \vartheta & i \sin \vartheta \\ i \sin \vartheta & \cos \vartheta \end{bmatrix} \text{ OK!}$$

Note that S_{11} and S_{22} are reflection coefficients for port 1 and 2 provided the other port is terminated by characteristic impedance

08-V-26

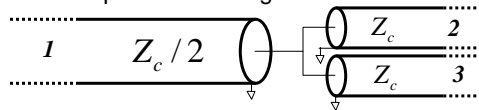
SYMMETRIES OF S MATRIX: CONSTRAINTS FOR LINEAR 3-PORT (NO PERFECT DIVIDER EXISTS)

THEOREM: IT IS IMPOSSIBLE FOR A NON-DISSIPATIVE 3-PORT TO BE SIMULTANEOUSLY POWER-MATCHING AND RECIPROCAL.

POWER- MATCHING: $\forall l, s_{ll} = 0$ RECIPROCITY: $'S = S$

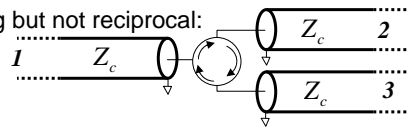
- Non-dissipative and reciprocal but not power matching:

$$s_{22} = s_{33} \neq 0$$



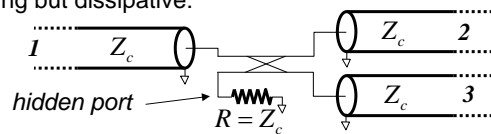
- Non-dissipative and power-matching but not reciprocal:

Circulator:



- Reciprocal and power-matching but dissipative:

Wilkinson divider:



08-V-27c

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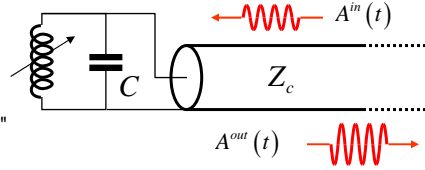
08-V-5e

ACTIVE LINEAR 1-PORT

B. Yurke, in "Quantum Squeezing", Springer (2004)

Simplest example:

$$L(t) = L + \delta L \sin(2\omega_0 t)$$



$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$\Gamma = \frac{1}{2Z_c C}$$

"Degenerate Parametric Amplifier"

$$\ddot{\Phi} + 2\Gamma\dot{\Phi} + \omega_0^2\Phi + i\omega_0^2\chi\Phi(e^{2i\omega_0 t} - e^{-2i\omega_0 t}) = 4\Gamma V^{in}(t) \quad V^{out}(t) = \dot{\Phi} - V^{in}(t)$$

Harmonic balance

$$\longrightarrow 2i\omega_0\Gamma\Phi[\omega_0] - i\omega_0^2\chi\Phi[-\omega_0] = 4\Gamma V^{in}[\omega_0]$$

After a few steps:

$$\begin{cases} A^{out}[\omega_0] = \frac{1+\zeta^2}{1-\zeta^2}A^{in}[\omega_0] + \frac{2\zeta}{1-\zeta^2}A^{in}[-\omega_0] \\ A^{out}[-\omega_0] = \frac{1+\zeta^2}{1-\zeta^2}A^{in}[-\omega_0] + \frac{2\zeta}{1-\zeta^2}A^{in}[\omega_0] \end{cases} \quad \zeta = \frac{1}{4} \frac{\delta L \omega_0}{L \Gamma} < 1$$

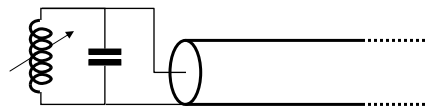
Generalized scattering matrix

$$\begin{bmatrix} A^{out}[\omega_0] \\ A^{out}[-\omega_0] \end{bmatrix} = \begin{bmatrix} c & s \\ s & c \end{bmatrix} \begin{bmatrix} A^{in}[\omega_0] \\ A^{in}[-\omega_0] \end{bmatrix} \quad c^2 - s^2 = 1$$

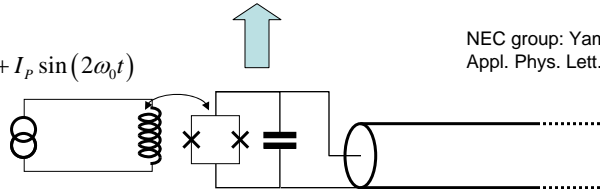
08-V-28c

NON-LINEAR CIRCUIT CAN BEHAVE LINEARLY FOR WEAK SIGNALS: SQUID

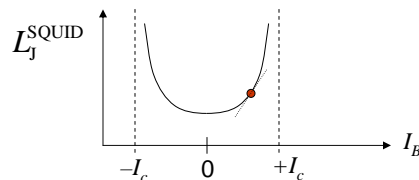
$$L(t) = L + \delta L \sin(2\omega_0 t)$$



$$I_B(t) = I_B + I_p \sin(2\omega_0 t)$$



NEC group: Yamamoto et al., Appl. Phys. Lett. 93, 042510 (2008)



IN THE VICINITY OF OPERATING POINT SQUID IS A VARIABLE INDUCTOR

08-V-29

SCATTERING MATRIX FOR ACTIVE LINEAR 2-PORTS

$$\begin{bmatrix} a_1^{out}[\omega_1] \\ a_1^{out}[-\omega_1] \\ a_2^{out}[\omega_2] \\ a_2^{out}[-\omega_2] \end{bmatrix} = \begin{bmatrix} r_1 & s_1 & t_{12} & u_{12} \\ s_1^* & r_1^* & u_{12}^* & t_{12}^* \\ t_{21} & u_{21} & r_2 & s_2 \\ u_{21}^* & t_{21}^* & s_2^* & r_2^* \end{bmatrix} \begin{bmatrix} a_1^{in}[\omega_1] \\ a_1^{in}[-\omega_1] \\ a_2^{in}[\omega_2] \\ a_2^{in}[-\omega_2] \end{bmatrix}$$

different frequencies

$$a[\omega] \sim \frac{1}{\sqrt{\omega}} A[\omega]$$

INFORMATION CONSERVATION \Rightarrow S MATRIX IS SYMPLECTIC ${}^t S J S = J$

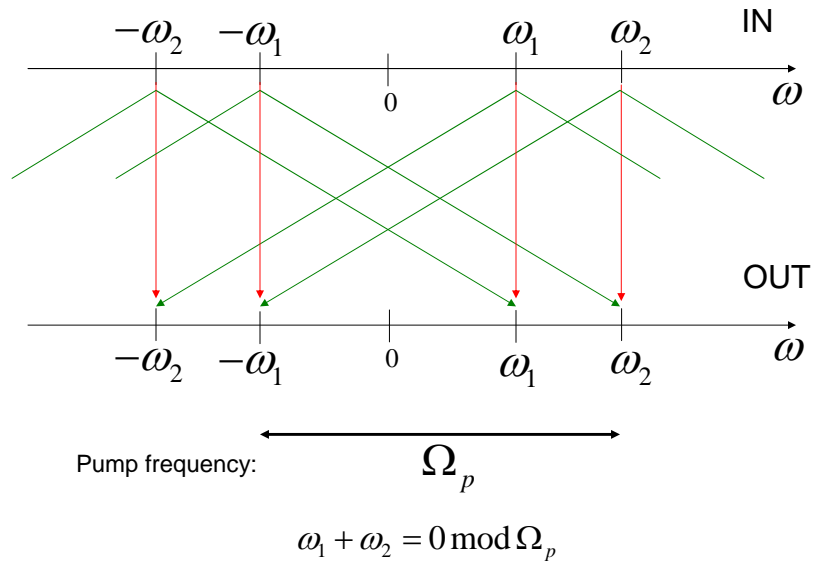
(ENERGY IS NOT CONSERVED, S IS NOT UNITARY)

$$J = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & 0 \end{bmatrix}$$

central to antisymmetric bilinear forms such as Poisson Brackets (and commutators)

08-V-31

IN NON-LINEAR ACTIVE DEVICES, SIGNALS CAN SCATTER BETWEEN DIFFERENT FREQUENCIES



08-V-30

TOPICS OF NEXT LECTURE:

1) AMPLIFICATION OF QUANTUM SIGNALS:
ULTIMATE SENSITIVITY

2) SQUEEZING OF QUANTUM NOISE

08-V-32

END OF LECTURE